



Geometria paletei

Ecuatii miscare



$l = 2.5 \mu m$	E = 150GPa
$a = 2\mu m$	$\nu = 0.17$
$b = 3.5 \mu m$	0 022013
d = 200 mm	$\rho = 2330 \text{kgm}^{-5}$
a = 200 nm	$f = 200 Nm^{-2}$
c = 175 nm	d asim =40nm



 $R \times R \ni (x, y, z, t) \rightarrow \{r(x, y, z, t), d_i(x, y, z, t)\} \in E^3$ $d_1 = (-\sin\psi\sin\varphi + \cos\psi\cos\varphi\cos\theta)e_1 + + (\cos\psi\sin\varphi + \sin\psi\cos\varphi\cos\theta)e_2 - \sin\theta\cos\varphi e_3,$ $d_2 = (-\sin\psi\cos\varphi - \cos\psi\sin\varphi\cos\theta)e_1 + + (\cos\psi\cos\varphi - \sin\psi\sin\varphi\cos\theta)e_2 + \sin\theta\sin\varphi e_3,$ $d_3 = \sin\theta\cos\psi e_1 + \sin\theta\sin\psi e_2 + \cos\theta e_3.$ $u_1 = \theta'\sin\varphi - \psi'\sin\theta\cos\varphi \qquad u_2 = \theta'\cos\varphi + \psi'\sin\theta\sin\varphi$ $u_3 = \tau = \varphi' + \psi'\cos\theta \qquad r = \int_0^s d_3 ds \qquad X(s) = \int_0^s \cos\psi\sin\theta ds$ $Y(s) = \int_0^s \sin\psi\sin\theta ds \qquad Z(s) = \int_0^s \cos\theta ds$ $s = k_1 x + k_2 y + k_3 z + \omega t$ Forme de echilibru ale barei incepand cu locul de imbinare cu paleta si terminand cu suportul



Forme de echilibru







	Mod translatie	
	ecuatie	frecventa [MHz]
Olkhovets 2001	$f_0 = 0.22 \sqrt{\frac{d^2 c}{l^3 b a} \frac{E}{\rho}}$	14.5
Dowell si Tang 2001 singur mod	$f_0 = 0.14 \sqrt{\frac{d^2 c}{l^3 b a} \frac{E}{\rho}}$	9.3
Dowell si Tang 2001 multi mod	$f_0 = 0.19 \sqrt{\frac{d^2 c}{l^3 b a} \frac{E}{\rho}}$	12.1
Duemling 2002	FEM- ANSIS	12.4
model neliniar CMP	Femlab	12.9
Experimental Evoy et al. 1999 Virginia Tech. Cornell Univ.		13.33 ± 0.05

Distributia tensiunilor (femlab) pt primele 4 moduri (translatie + incovoiere + torsiune)





Concluzii

- 1. Se analizeaza paleta nanorezonanta. Paleta poate detecta deformatii la scara nanometrica, fapt pentru care este ideala pentru studiul proprietatilor electromagnetice si mecanice ale nanomaterialelor.
- 2. Spre deosebire de teoriile existente (in care paleta este considerata rigida si se scriu si se trateaza separat ecuatiile pentru translatie, incovoiere sau torsiune), in aceasta lucrare atat barele cat si paleta sunt corpuri elastice deformabile. Miscarea paletei este tratata *unitar*, scriindu-se un *singur set de ecuatii exacte neliniare ale miscarii paletei*. Se utilizeza *teoria solitonilor* pentru determinarea *solutiilor exacte ale acestor ecuatii*.
- 3. Noutatea lucrarii consta in determinarea primelor frecvente de rezonanta si a modurilor asociate. Rezultatele sunt mai apropiate de datele experimentale decat ale altor teorii, deoarece frecventele calculate nu reprezinta separat frecvente de translatie, incovoiere sau torsiune, ci reprezinta *unitar*, ca si in experiment, frecventele de rezonanta ale paletei.
- 4. Noutatea lucrarii consta in analiza ruperii barei la imbinarea cu paleta cu ajutorul *teoriei dilatonilor*

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